



Real-Time Attack-Recovery for Cyber-Physical Systems Using Linear Approximations

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Motivation

CPS attacks **cannot** be handled by **classic cyber security mechanisms**

Sensor spoofing attack

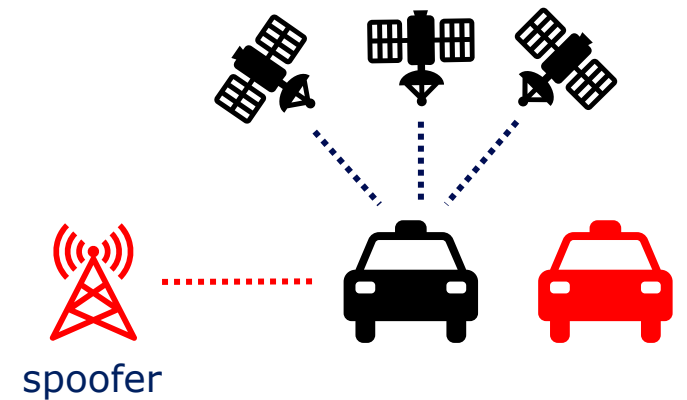
- software attacks

malicious sensor information

drive the **physical system** to unsafe state

- transduction attacks

manipulates a **physical property** that affects sensor reading



Motivation

Most of the literature focus on attack-detection

- 32 recent CPS security surveys
 - **most of them** talked about **attack-detection**
 - only 8 of them described response to attacks

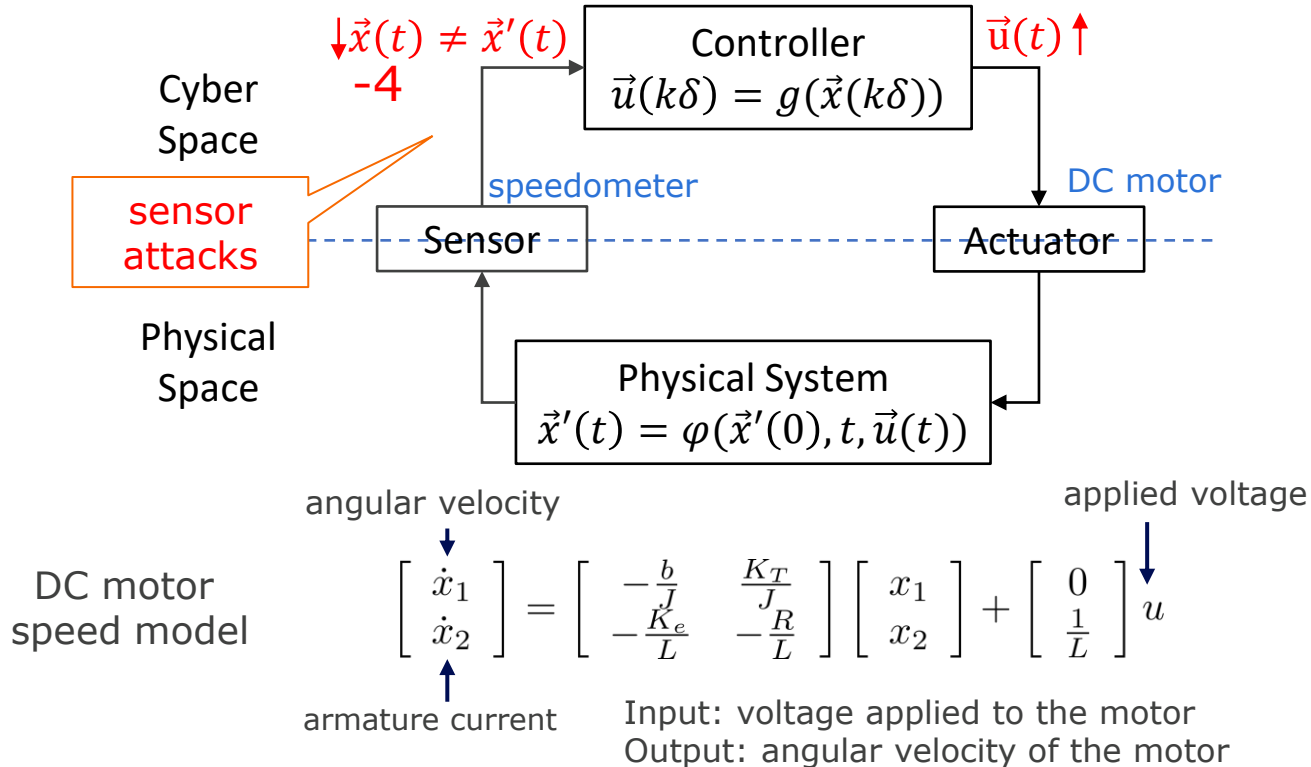
After detecting an attack, what should we do?

This paper focuses on **attack recovery** in a real time manner

Motivational Example

Cruise Control

Control stepsize δ : 0.02s



Attack scenarios:

(1) Modification:

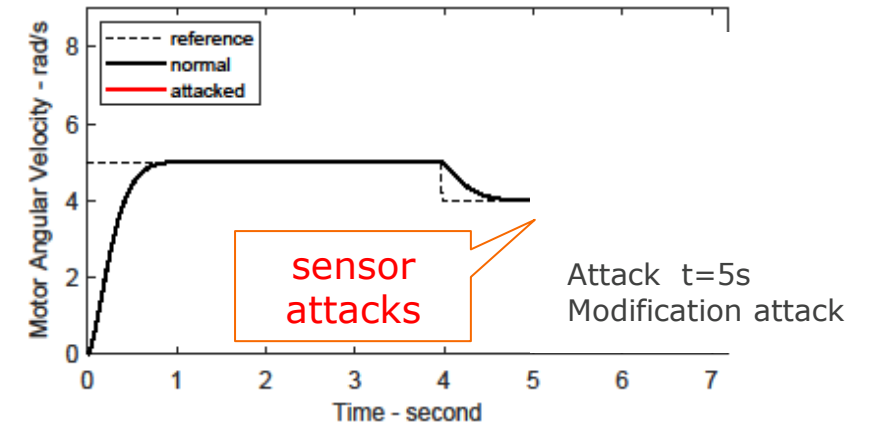
adding/subtracting some values

(2) Replay:

use data from previous time period

(3) Delay:

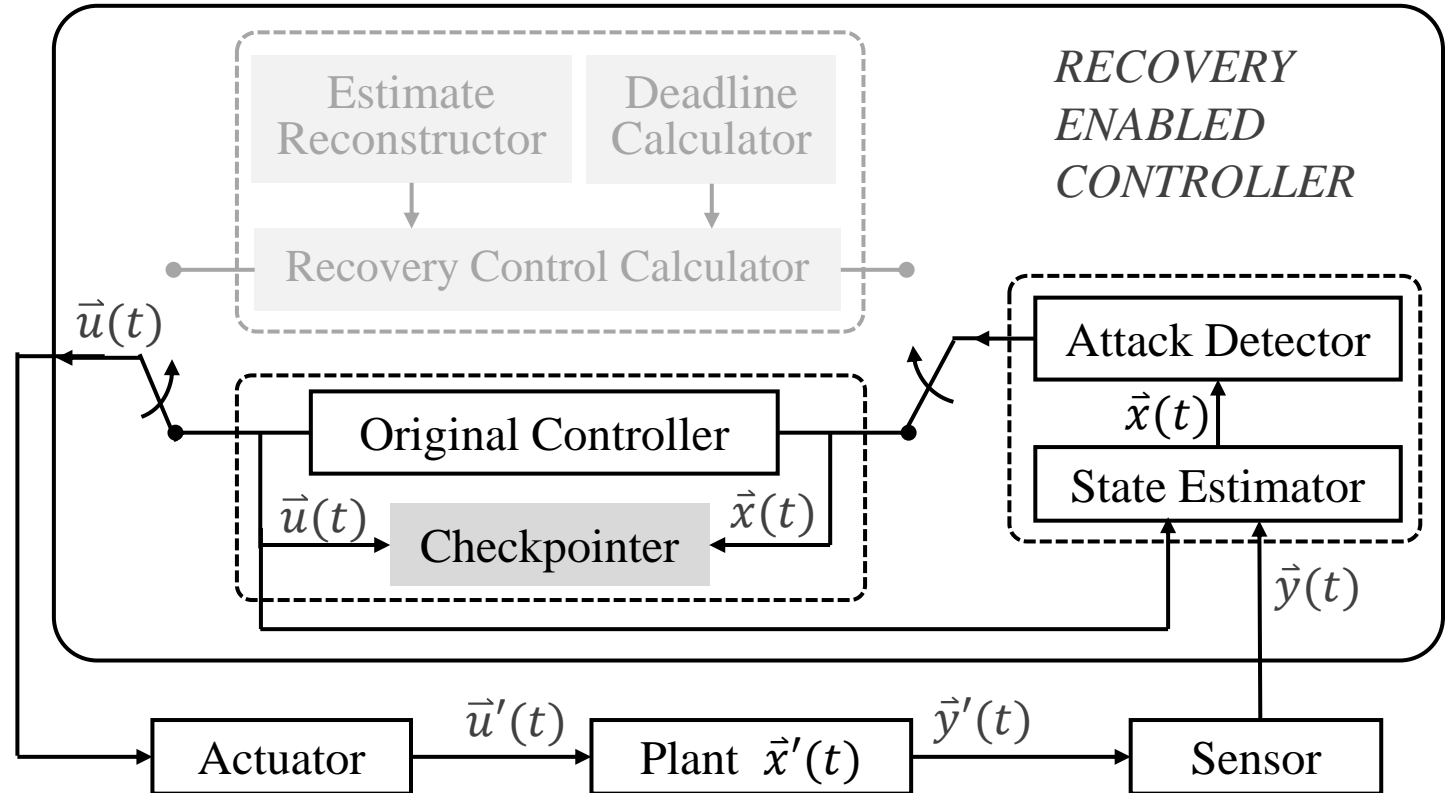
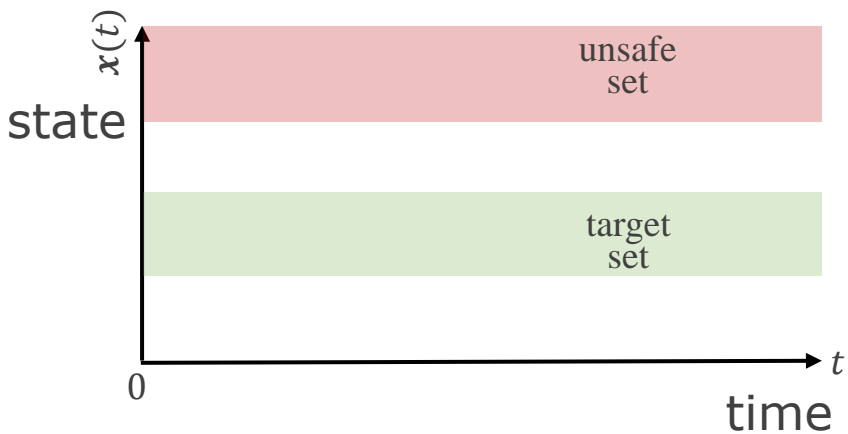
intentionally delay the data



Overview of the Real-Time Recovery Framework

Unsafe set: the set of states that define catastrophic events.

Target set: the set of desired states. E.g., planned paths, reference values.



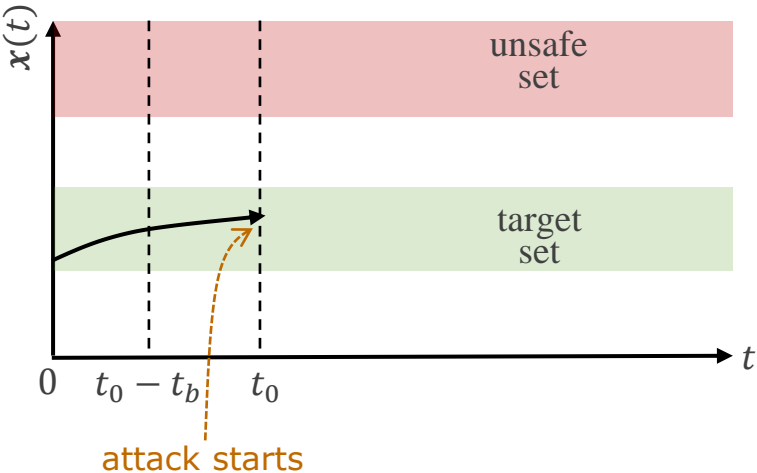
Overview of the Real-Time Recovery Framework

original controller

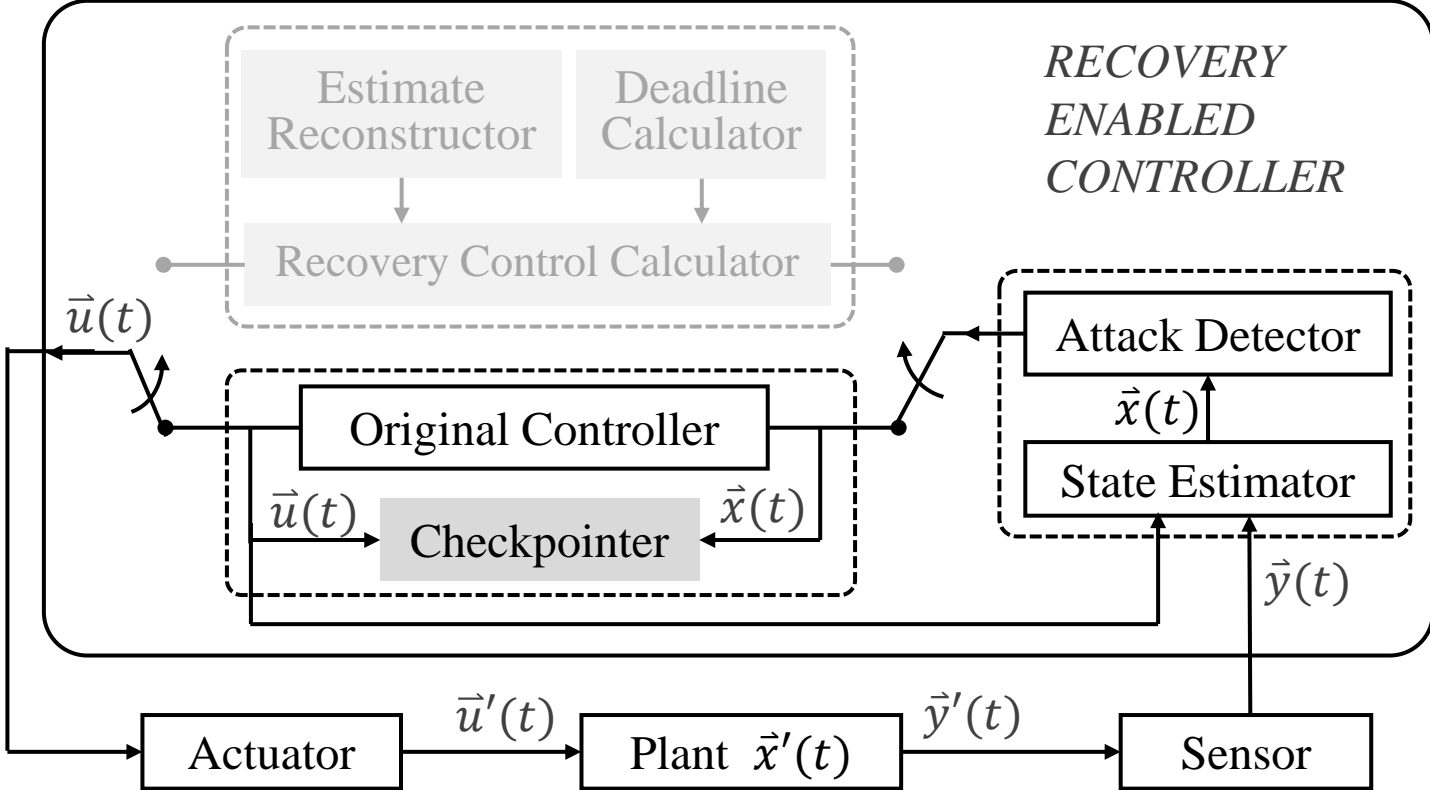
checkpointer

- record historical data
 - state estimate $\vec{x}(t)$
 - control input $\vec{u}(t)$

an attack is launched at t_0



Normal Mode



Overview of the Real-Time Recovery Framework

attack is detected after at most t_a

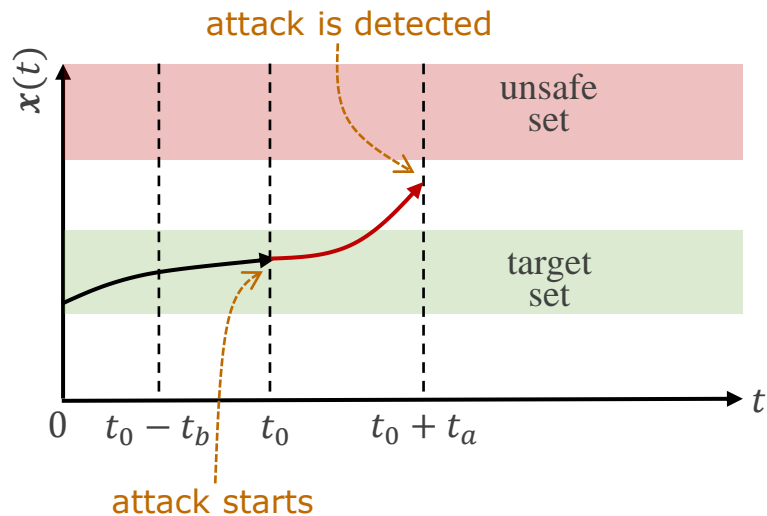
- switch to the recovery mode

estimate reconstructor

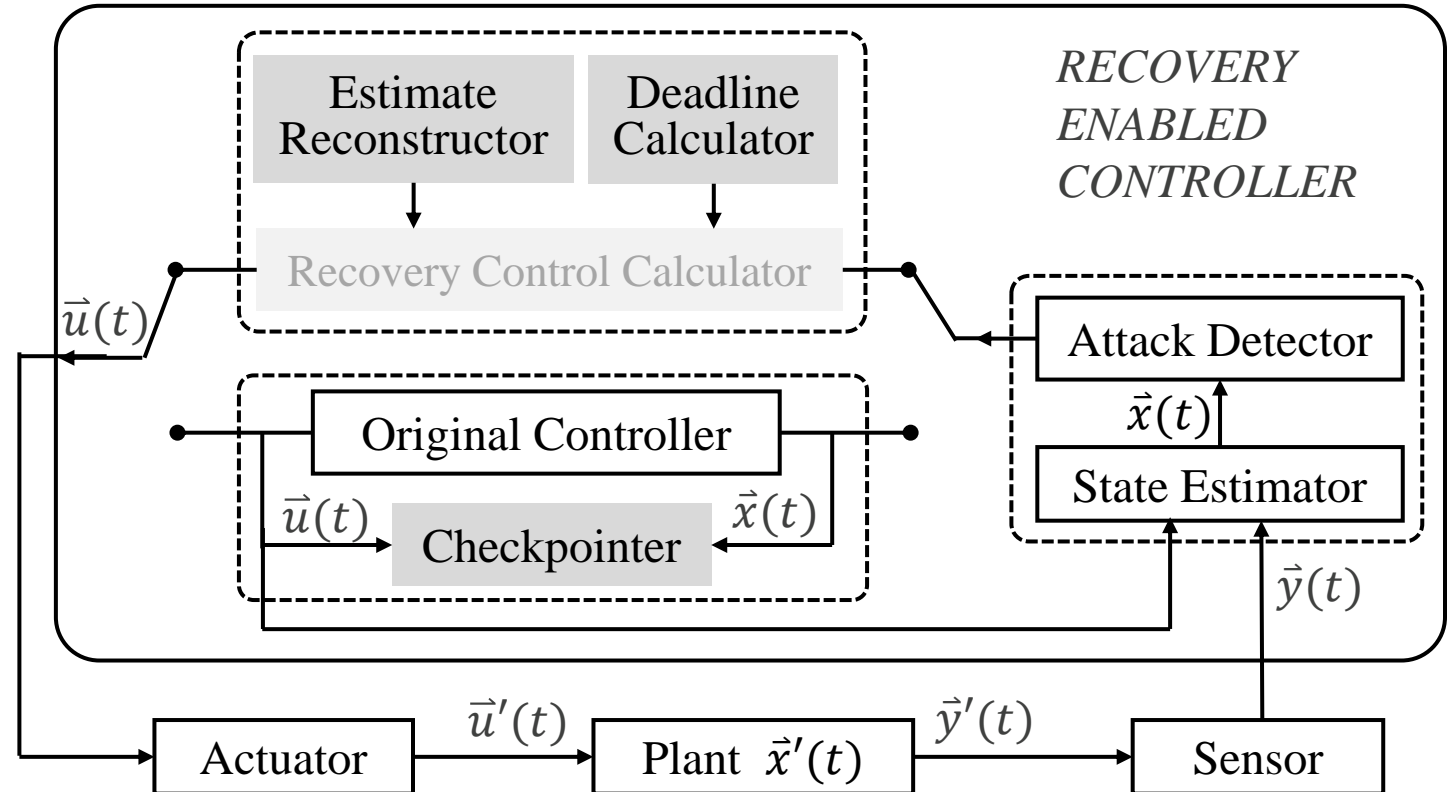
- rebuild state estimate at $t_0 + t_a$

deadline calculator

- calculate a safety deadline t_d



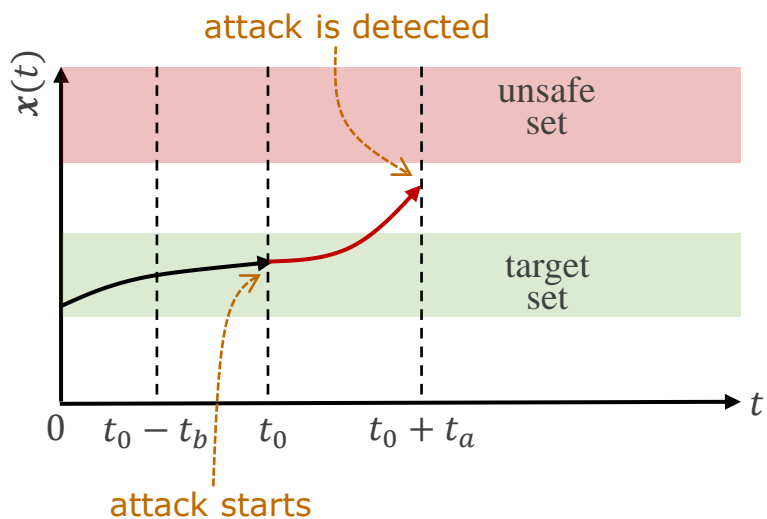
Recovery Mode



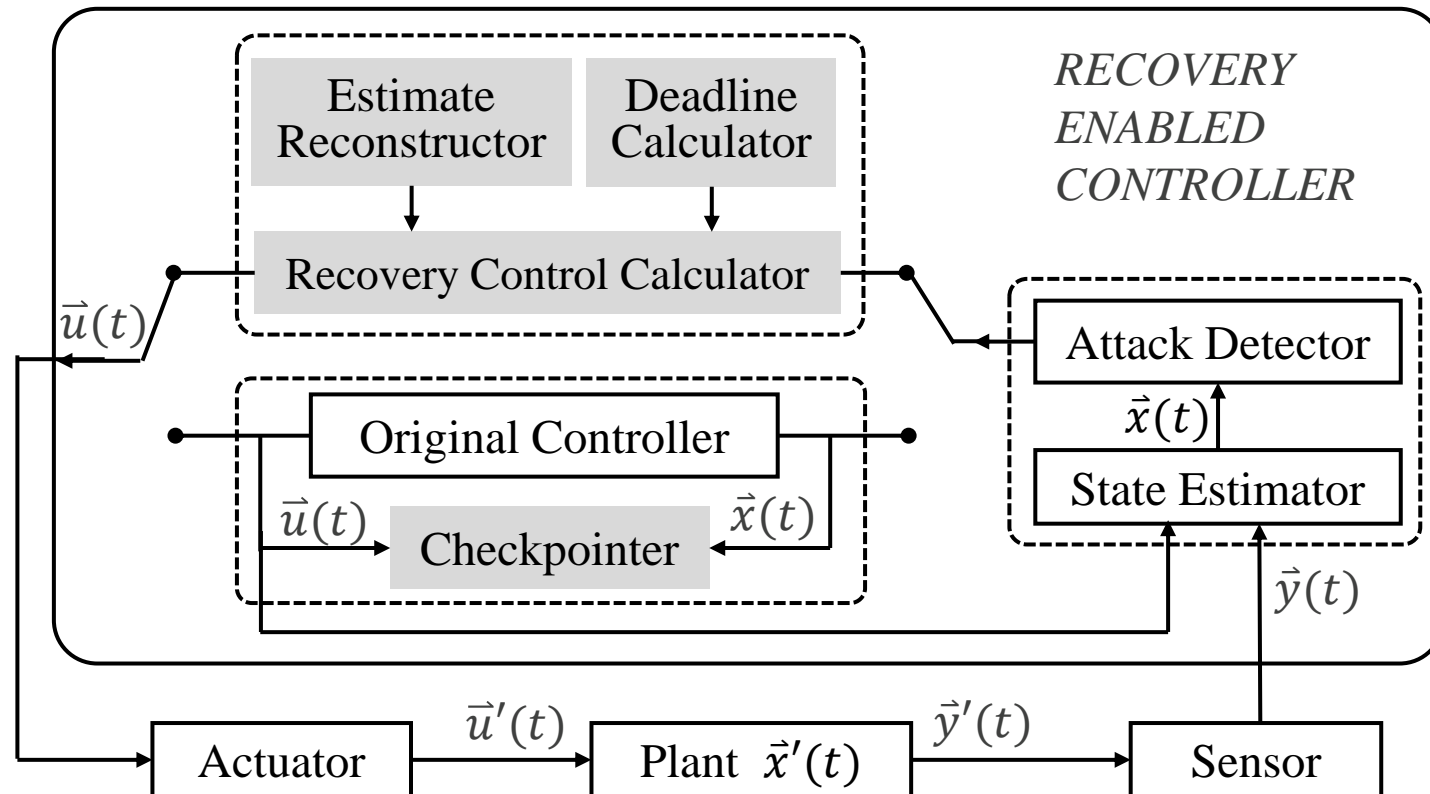
Overview of the Real-Time Recovery Framework

recovery control calculator

- compute a Piece-Wise Constant control sequence
 - rebuilt state \rightarrow target set
 - within safety deadline



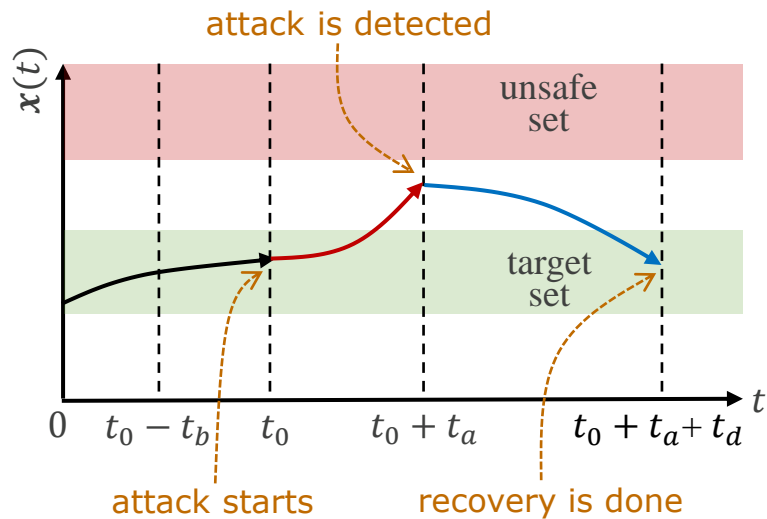
Recovery Mode



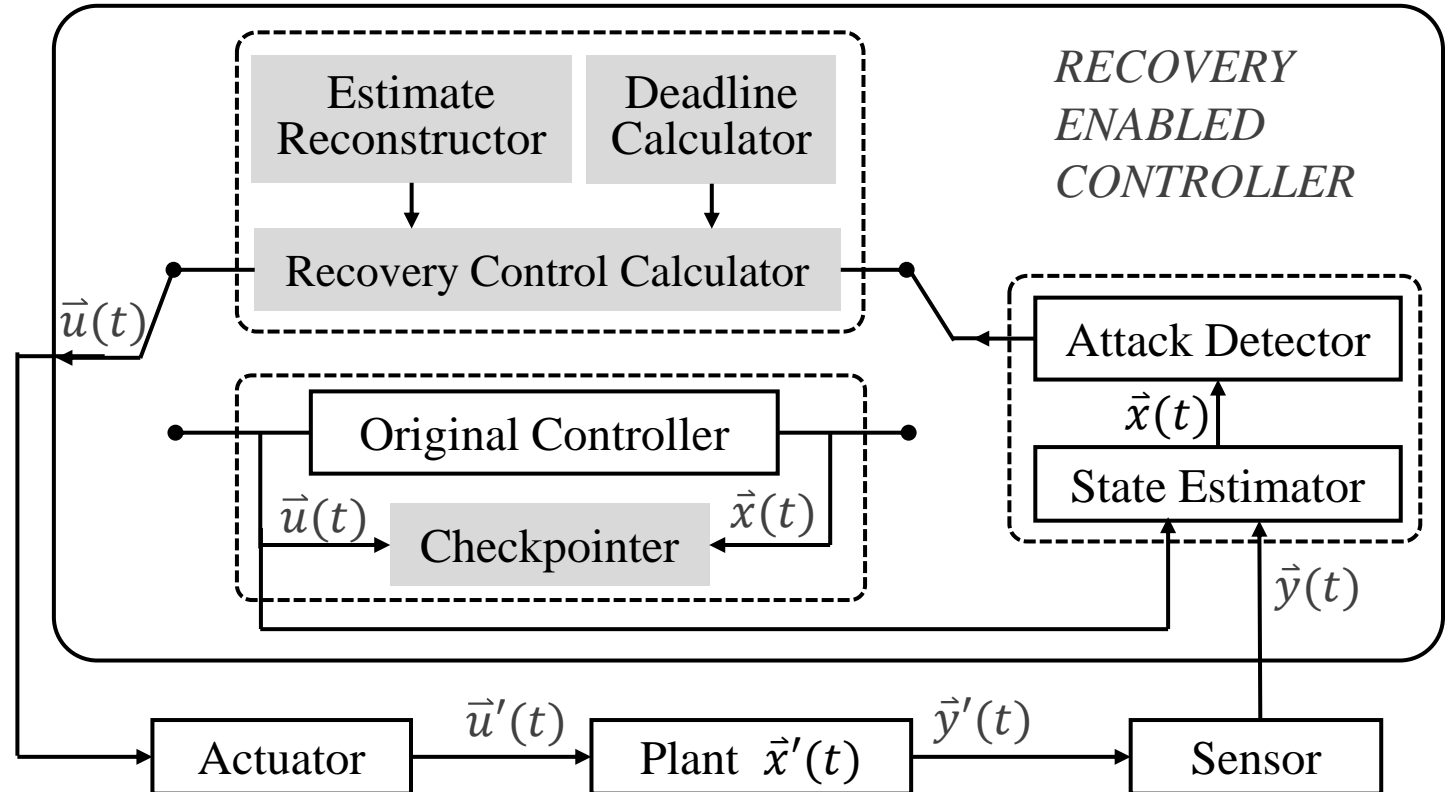
Overview of the Real-Time Recovery Framework

recovery controller

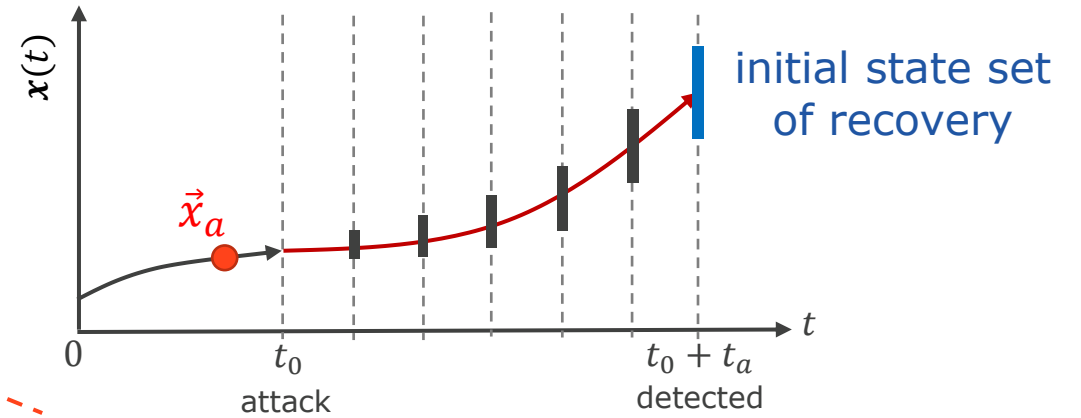
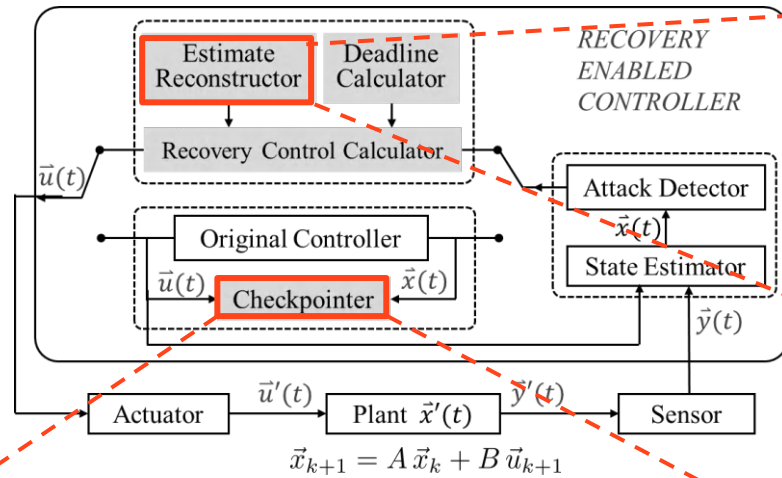
- apply recovery control sequence immediately
- back to target state set before $t_0 + t_a + t_d$



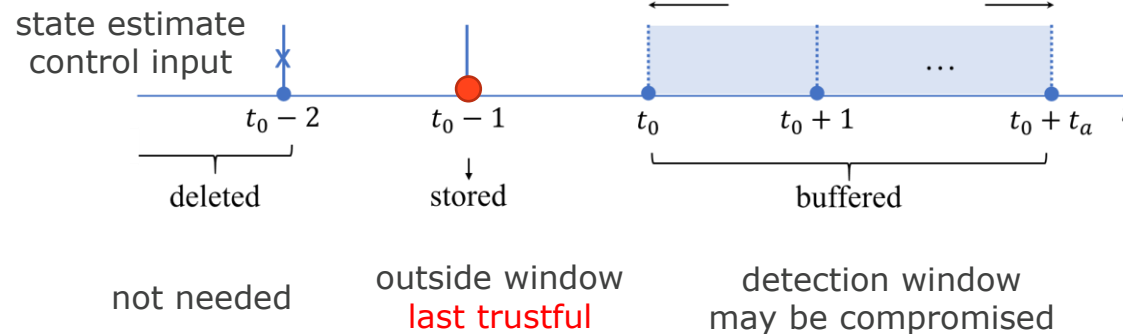
Recovery Mode



Estimate Reconstructor



checkpoint protocol



plant ϵ -LTI approximation

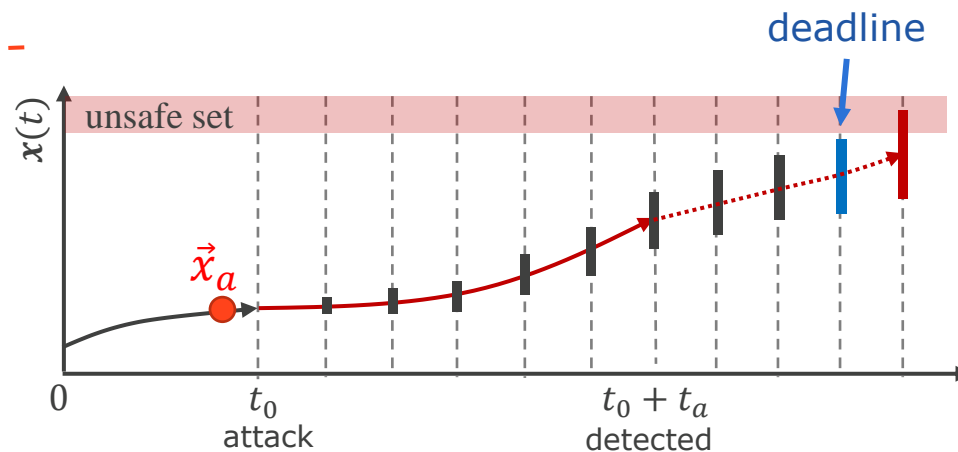
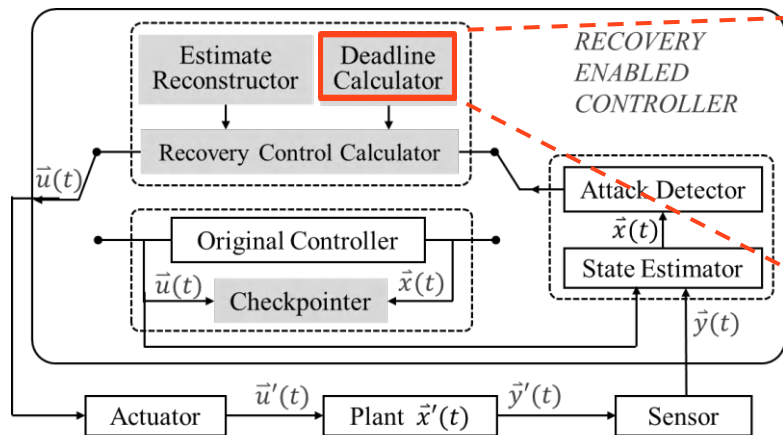
$$\varphi(\vec{s}, \delta, \vec{c}) \in \{A\vec{s} + B\vec{c}\} \oplus \mathcal{B}_\epsilon \quad (2)$$

reachable state set at time $t_0 + t_a$

$$\left\{ A^{N_a} \vec{x}_a + \sum_{j=0}^{N_a-1} A^j B \vec{c}_{N_a-j} \right\} \oplus \bigoplus_{j=0}^{N_a-1} A^j \mathcal{B}_\epsilon \quad (4)$$

box overapproximation – support function method

Deadline Calculator



Reachability computation:

$$Z_i = \left\{ A^{N_a+i} \vec{x}_a + \sum_{j=i}^{N_a+i-1} A^j B \vec{c}_{N_a+i-j} \right\} \oplus \bigoplus_{j=0}^{N_a+i-1} A^j \mathcal{B}_\epsilon \oplus \underbrace{\left\{ \sum_{j=0}^{i-1} A^j B \vec{c}_{N_a+i-j} \right\}}_{\Phi_i}$$

where future control input $\vec{c}_{N_a+1}, \dots, \vec{c}_{N_a+i}$ is pre-assumed

Safety checking based on support function:

$$a_p^T A^{N_a+i} \vec{x}_a + \sum_{j=0}^{N_a+i-1} a_p^T A^j B \vec{c}_{N_a+i-j} + \sum_{j=0}^{N_a+i-1} \sqrt{a_p^T A^j (A^j)^T a_p} \epsilon \stackrel{?}{>} b.$$

support function of a set $S \subseteq \mathbb{R}^n$ according to a vector \vec{l} :

$$\rho_S(\vec{l}) = \sup_{s \in S} \{ \vec{l}^T s \}$$

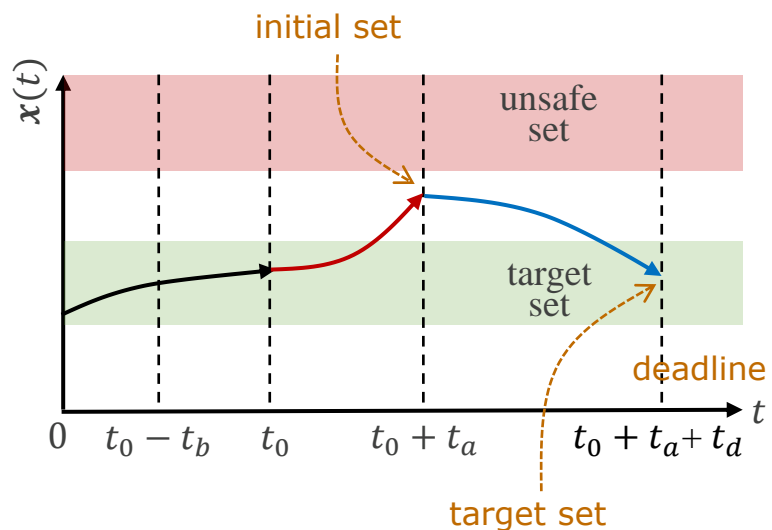
For support function on convex sets

$$\begin{aligned} \rho_{AS}(\vec{l}) &= \rho_S(A^T \vec{l}), & \text{for convex set } S \\ \rho_{S_1 \oplus S_2}(\vec{l}) &= \rho_{S_1}(\vec{l}) + \rho_{S_2}(\vec{l}) & \text{for convex sets } S_1, S_2 \end{aligned}$$

For $\Omega_j = A^j \mathcal{B}_\epsilon$, we have

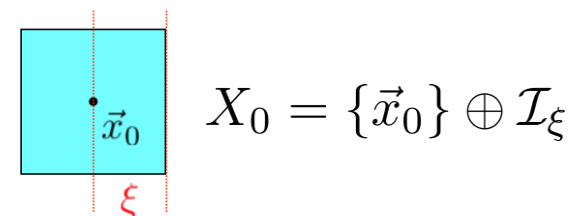
$$\rho_{\Omega_j}(\vec{l}) = \sqrt{\vec{l}^T A^j (A^j)^T \vec{l}} \epsilon$$

Real-time Recovery using PWC Control



the recovery problem asks whether there exists a **recovery control sequence** $\vec{u}_1, \dots, \vec{u}_N$ where $N \leq D$ steering the system from **initial state** \vec{x}_0 to a state in **target set** X_T while all reachable states on the way are in a **safe set** X_S .

Linear Programming Problem



single initial set

extension to an initial set

Find $\vec{u}_1, \dots, \vec{u}_D \in \mathcal{U}$

$$\begin{aligned} \text{s.t. } \vec{x}_D \in X_T & \longrightarrow \vec{x}_D \in (X_T \ominus A^D \mathcal{I}_\xi) \\ \bigwedge_{i=0}^D (\vec{x}_i \in X_S) & \longrightarrow \bigwedge_{i=0}^D \vec{x}_i \in (X_S \ominus A^i \mathcal{I}_\xi) \\ \bigwedge_{i=0}^{D-1} (\vec{x}_{i+1} = A\vec{x}_i + B\vec{u}_{i+1}) & \end{aligned}$$

states in target set is maintainable

$\forall \vec{s} \in X_T$ is maintainable, iff.

$$(I - A)\vec{s} = B\vec{c}, \text{ i.e., } \vec{s} = A\vec{s} + B\vec{c}$$

Evaluation - Benchmarks

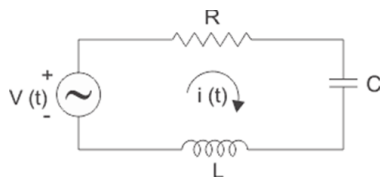
1. Vehicle Turning

$$\dot{x} = -\frac{25}{3}x + 5u$$



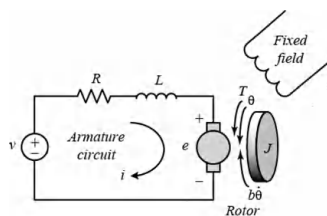
2. Series RLC Circuit

$$\begin{bmatrix} \dot{x}_1 \\ \dot{x}_2 \end{bmatrix} = \begin{bmatrix} 0 & \frac{1}{C} \\ -\frac{1}{L} & -\frac{R}{L} \end{bmatrix} \begin{bmatrix} x_1 \\ x_2 \end{bmatrix} + \begin{bmatrix} 0 \\ \frac{1}{L} \end{bmatrix} u$$



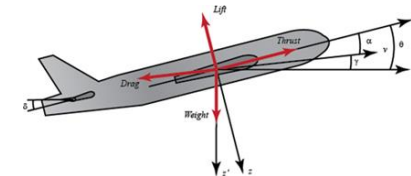
3. DC Motor Position

$$\begin{bmatrix} \dot{x}_1 \\ \dot{x}_2 \\ \dot{x}_3 \end{bmatrix} = \begin{bmatrix} 0 & 1 & 0 \\ 0 & -\frac{b}{J} & \frac{K}{J} \\ 0 & -\frac{K}{L} & -\frac{R}{L} \end{bmatrix} \begin{bmatrix} x_1 \\ x_2 \\ x_3 \end{bmatrix} + \begin{bmatrix} 0 \\ 0 \\ \frac{1}{L} \end{bmatrix} u$$



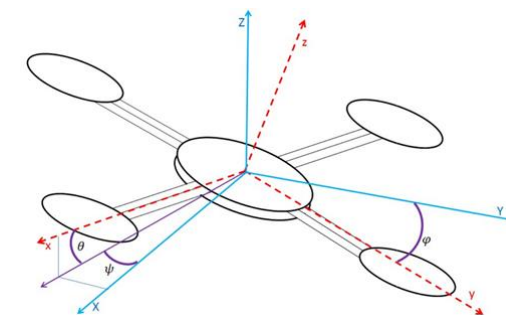
4. Aircraft Pitch

$$\begin{bmatrix} \dot{x}_1 \\ \dot{x}_2 \\ \dot{x}_3 \end{bmatrix} = \begin{bmatrix} -0.313 & 56.7 & 0 \\ -0.0139 & -0.426 & 0 \\ 0 & 56.7 & 0 \end{bmatrix} \begin{bmatrix} x_1 \\ x_2 \\ x_3 \end{bmatrix} + \begin{bmatrix} 0.232 \\ 0.0203 \\ 0 \end{bmatrix} u$$

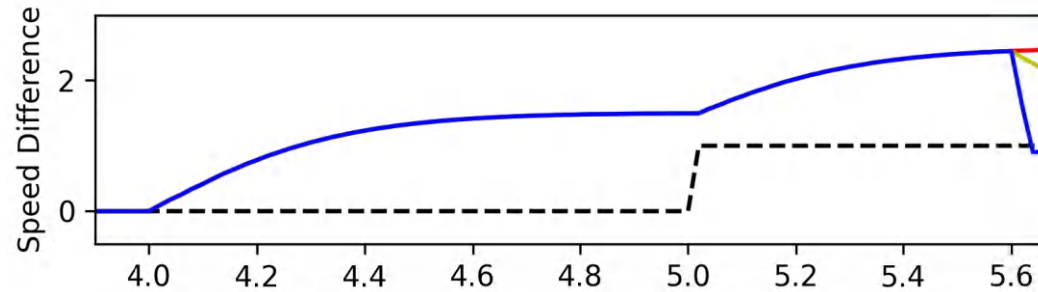


5. Quadrotor

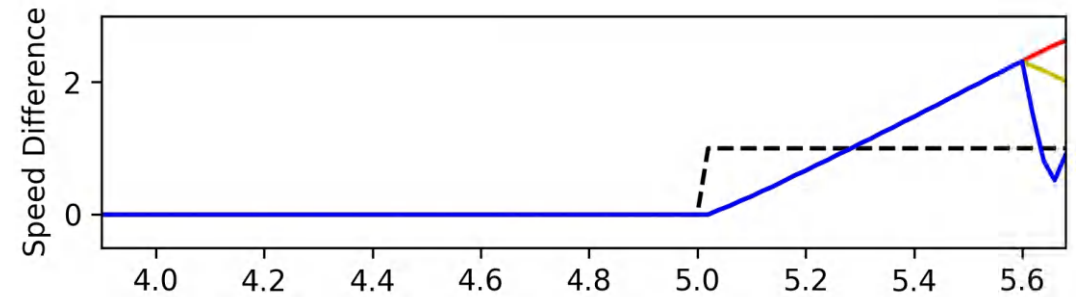
$$\begin{cases} \dot{\phi} = p \\ \dot{\theta} = q \\ \dot{\psi} = r \\ \dot{p} = \frac{\tau_x + \tau_{wx}}{I_x} \\ \dot{q} = \frac{\tau_y + \tau_{wy}}{I_y} \\ \dot{r} = \frac{\tau_z + \tau_{wz}}{I_z} \\ \dot{u} = -g\theta + \frac{fwx}{m} \\ \dot{v} = g\phi + \frac{fwy}{m} \\ \dot{w} = \frac{fwz - ft}{m} \\ \dot{x} = u \\ \dot{y} = v \\ \dot{z} = w \end{cases}$$



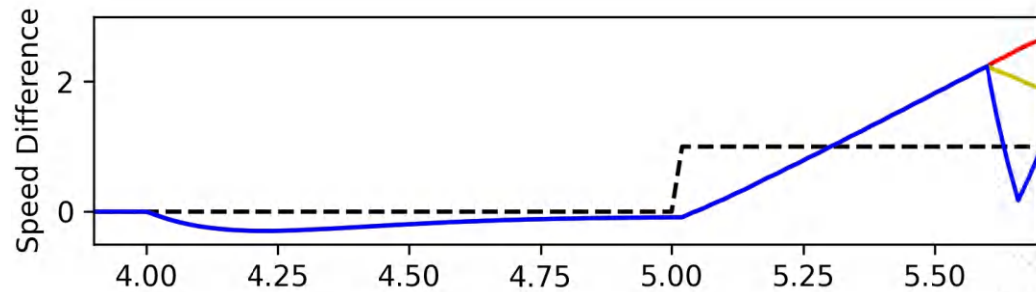
Evaluation – Results for Vehicle Turning



(a) Vehicle turning & modification attack



(b) Vehicle turning & delay attack



(c) Vehicle turning & replay attack

our method can do real-time recovery

Legend:

Dotted Black: Reference state

Red: No recovery

Yellow: Non-real-time recovery

Blue: Real-time recovery

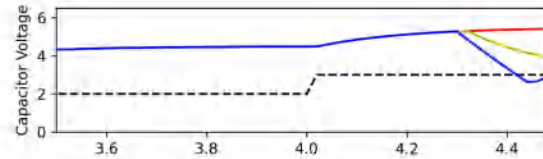
Evaluation – Other Results

Modification

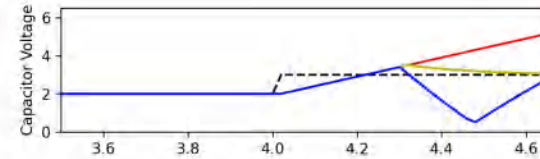
Delay

Replay

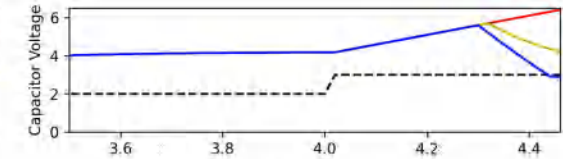
RLC Circuit



(d) RLC Circuit & modification attack

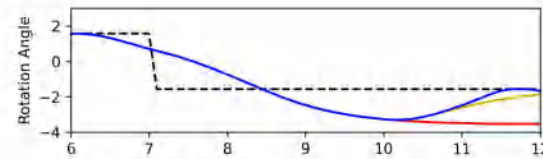


(e) RLC Circuit & delay attack

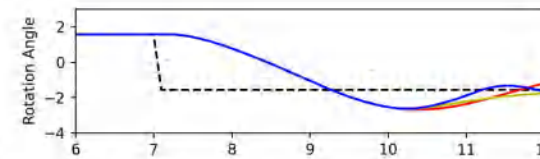


(f) RLC Circuit & replay attack

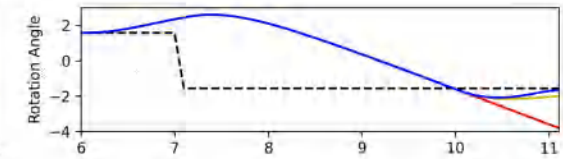
DC Motor Position



(g) DC Motor Position & modification attack

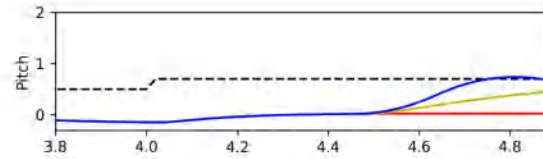


(h) DC Motor Position & delay attack

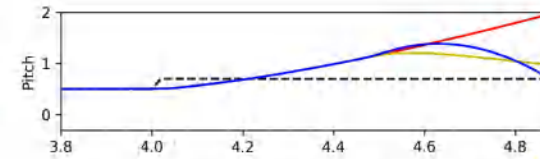


(i) DC Motor Position & replay attack

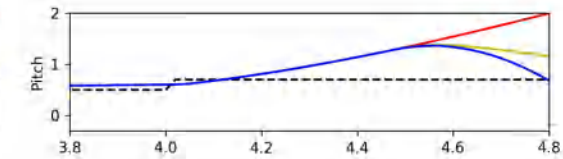
Aircraft Pitch



(j) Aircraft Pitch & modification attack

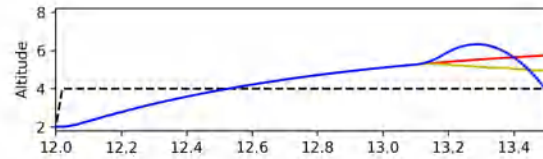


(k) Aircraft Pitch & delay attack

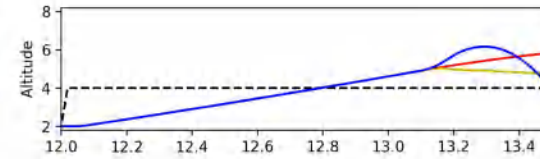


(l) Aircraft Pitch & replay attack

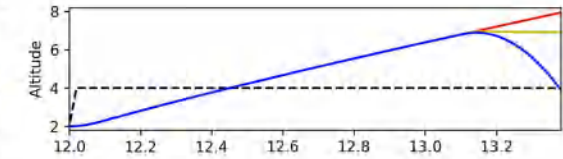
Quadrotor



(m) Quadrotor & modification attack



(n) Quadrotor & delay attack



(o) Quadrotor & replay attack

Evaluation – Time Cost

overhead is small

B	δ	A	k	X_0	T_D	T_F	T_S	Total	%
#1	20	M	3	0.35	0.29	0.07	0.03	0.74	3.71%
		D	4	0.34	0.35	0.06	0.02	0.77	3.84%
		R	5	0.34	0.41	0.07	0.03	0.85	4.24%
#2	20	M	9	0.34	0.67	0.22	0.07	1.30	6.52%
		D	18	0.34	1.62	0.41	0.14	2.49	12.46%
		R	8	0.31	0.65	0.12	0.06	1.14	5.69%
#3	100	M	20	0.53	1.59	1.00	0.28	3.40	3.40%
		D	20	0.28	1.54	1.70	0.29	3.81	3.81%
		R	11	0.33	0.90	0.41	0.12	1.76	1.76%
#4	20	M	21	0.34	2.02	0.97	0.31	3.64	18.21%
		D	21	0.36	2.02	1.50	0.29	4.17	20.86%
		R	17	0.35	1.43	0.75	0.21	2.74	13.69%
#5	20	M	20	0.53	1.81	7.52	1.14	11.0	55.01%
		D	20	0.43	1.75	7.38	1.14	10.70	53.55%
		R	14	0.50	1.48	3.49	0.59	6.06	30.28%

Evaluation – Scalability Analysis

Scalable Heating Model

heating in a point of a rod located at **1/3** of the length

recording the temperature at **2/3** of the length

of variables is scalable $n = 25, 30, 35, 40, 45$

overhead increase with # of variables

The temperatures of the selected points on the rod is described by

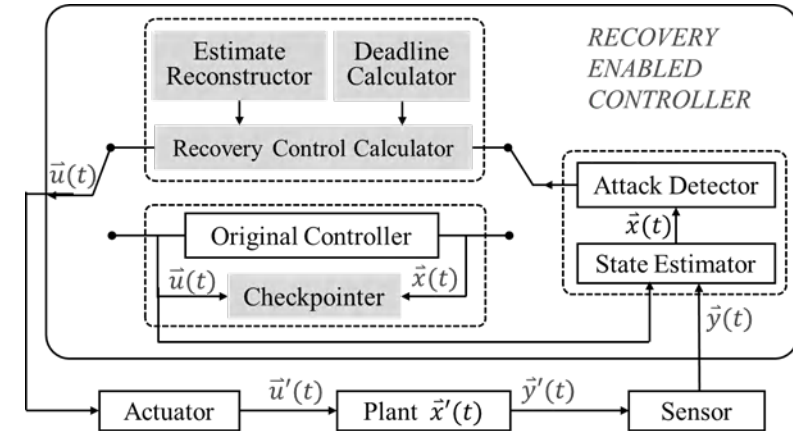
$\dot{\vec{x}} = A\vec{x} + Bu$ such that

$$A = \frac{\alpha}{h^2} \begin{pmatrix} 2 & -1 & & & & & \\ -1 & 2 & -1 & & & & \\ & \ddots & \ddots & \ddots & & & \\ & & & -1 & 2 & -1 & \\ & & & & -1 & 2 & \\ & & & & & -1 & 2 \end{pmatrix}$$

n	X_0	T_D	T_F	T_S	Total	%
20	0.57	0.96	17.37	4.99	23.89	11.94%
25	0.57	0.99	41.26	6.95	49.77	24.88%
30	0.63	1.03	59.59	8.00	69.25	34.62%
35	0.66	1.11	74.64	10.22	86.63	43.32%
40	0.74	1.17	81.77	13.15	96.83	48.42%
45	0.75	1.28	86.68	17.23	105.94	52.97%

Summary

- A new attack-recovery architecture
 - estimate reconstructor
 - deadline calculator
 - recovery control calculator



- A formal method to conservatively **estimate** the current and future states with a control **stepwise error bound** $\varepsilon > 0$ based on a Linear Time-Invariant (**LTI**) approximate
- Formulate the **reach-avoid problem** as a **Linear Programming (LP)** restriction with safety and target specifications
- Formal analysis + Simulation + Scalability analysis



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Thank you.
Q&A

